NORTH DAKOTA DEPARTMENT OF TRANSPORTATION

MATERIALS AND RESEARCH DIVISION

Experimental Study ND 2001-01

Use of Stainless Steel Alternative for a Corrosion Resistance Structure

Construction Report

Project IM-2-094(011)289

November 2001

Preparedby

NORTH DAKOTA DEPARTMENT OF TRANSPORTATION BISMARCK, NORTH DAKOTA Website:http://discovernd.com/dot

> DIRECTOR Dave Sprynczynatyk

MATERIALS AND RESEARCH DIVISION Ron Horner

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Rhaub Walker

Disclaimer

The contents of this report reflect the views of the author or authors who are responsible for the facts and the accuracy of the data presented herein. The contents do not reflect the official views of the North Dakota Department of Transportation or the Federal Highway Administration. This report does not constitute a standard, specification, or regulation.

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Use of Stainless Steel Alternative for a Corrosion Resistance Structure

<u>Objective</u>

The deterioration of reinforced concrete structures has long been a problem to highway agencies. The major cause of the deterioration results from corrosion of the steel due to chlorides.

The cost of using stainless steel rebar is prohibitive for highway construction at this time but a new product known as Nuovinox, a carbon steel rebar clad with stainless steel is reported to be a stainless steel alternative priced considerably lower than stainless steel.

The objective of this research study is to determine if a carbon steel rebar clad with stainless steel is a cost effective new method of combating the effects of chloride intrusion.

Reinforcing steel is protected in concrete by a passive iron oxide layer that forms because of the high pH of the concrete. Corrosion won't occur as long as there are no breaks in the passive layer over the steel. The layer may be broken by two things; one involves carbonation, the other, chloride ions.

Carbonation occurs when carbon dioxide from the air reacts with water to form a weak acid that converts calcium hydroxide within the hydrated cement paste to calcium carbonate. Given time, this reaction can work its way in from the surface of the concrete to the reinforcing steel, reduce the pH of the concrete surrounding the steel, and allow corrosion to begin. However, with a low water to cement ratio, carbonation is seldom a concern.

Most corrosion problems are related to chlorides. It has been noted that the formation of an iron chloride complex ion frees the iron to begin the corrosion process. When the concentration of chlorides gets higher than a threshold level, corrosion starts.

1

Corrosion has been attributed to the fact that chloride destroys the protective passivation film which is formed on steel surfaces due to the high pH condition in concrete pore solution (pH=12-13).

Research on concrete durability has greatly increased and has demonstrated that many of severe problems, such as cracking, delamination and spalling of concrete, are related to chloride induced steel corrosion. The corrosion induced damage is a serious problem for the structure.

<u>Scope</u>

The plans for this project call for the use of a stainless steel clad rebar for its reinforcing steel. The use of this product is limited and ongoing research in many states is being conducted. Unlike epoxy coated rebar, its cladding is resistant to accidental damage and bars can be mechanically handled in the same way as black bars. It can be field bent, cut, and welded. Its chloride threshold is the same as solid stainless. If the coating on epoxy rebar is nicked during transport or installation, resulting in a damage level of only 5%, the chlorine threshold of the damaged bar becomes the same as black bar. Corrosion will then continue underneath the damaged epoxy coating. Typically, epoxy rebar will give corrosion protection for an average of 10 years. The advertised projected life span for stainless steel clad rebar is 75-100 years.

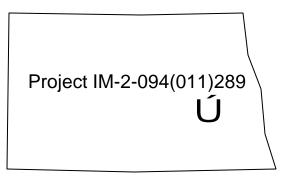
Precleaned epoxy coated reinforcing bars are protected with a coating of powdered epoxy that's fusion-bonded to the steel in an assembly fine process. Typically, manufacturers have the capability to coat straight bars, but only a few can coat bent bars. The coating physically blocks chloride ions. However, unless the bars are coated after bending, there's a potential for cracking and chipping of the epoxy coating during bending. Damage to the epoxy coating also may occur during field-handling of the bars.

2

Location

The bridge is located West of Valley City, North Dakota, on Interstate 94 in reference mile 290. The National Bridge Number is 94-290.803. The project number is IM-2-094(011)289.

The West Valley City Interchange bridge is 0.025 Miles long. The project begins at station 5353+67.69 and ends at 5354+98.69.



Project History

Construction

Construction history at the location of the project is shown in Table 1.

Year	Туре	Width (feet)		
1958	Structure	40.0		
1979	Approach Slab	-		
1979	PCC Deck Overlay	-		
1985	RailRetrofit	-		
2001	Structure	40.0		

Traffic

Traffic data at the location of the project is shown in Table 2.

		Design Data		
Traffic		Average Daily		Est. Max Hr. 490
Current 2000	Pass: 4115	Trucks 775	Total4890	490



<u>Design</u>

Construction of two structures on Interstate 94 near Valley City is proposed for the Year 2000. One structure will be constructed using epoxy coated rebar as specified by NDDOT specifications and the other structure will use the Nuovinox rebar during construction. The amount of rebar in each structure is approximately 44,000 pounds.

Test Structure

The work at this site consists of building a new 131 foot long, 3-span spread box girder bridge with a clear roadway width of 40 feet.

The NDDOT project engineer is Mike Flaagan and the NDDOT bridge engineer is Terry Udland. The contractor for this project is Industrial Builders Inc.

The stainless steel clad reinforcing to be used in the superstructure shall be Stelax Nuovinox316L Clad Rebar Grade 60 from Stelax Industries Ltd. The reinforcing bar list and details for the test structure are located in Appendix A. Photo 1 shows an example of a stainless steel clad rebar. The rebar is manufactured in South Wales, United Kingdom.



Photo 1. Example of Stainless Steel Clad Rebar

Control Structure

The bridge is located West of Valley City. The project number for the control section is IM-2-094(043)289. The bridge begins at Station 5353+74 and ends at Station 5355+05.

The National Bridge Number is 94-290.803L-3. The bridge was constructed in May of 2000 and the contractor was Industrial Builders Inc.

The type of reinforcing steel used within the bridge deck was epoxy coated rebar.

<u>Material</u>

The following statements are from the manufacturers literature.

Nuovinox 316L is available in Grades 300 MPa, 420 MPa & 520 MPa (Grades 40, 50 & 75) and conforms to ASTM A 615 and ASTM A 955. The outer stainless layer is made from 316L which is an austenitic chrome nickel alloy with Molybdenum. The composition of the inner core can vary depending on the application, for example the Grade size.

The stainless steel clad rebar is made through a patented green process which results in a metallurgical bond during hot-rolling between its outer stainless steel cladding and its carbon steel core. The process is unique in the fact that the cladding is not installed after the bar is made but rather at the point of its conception. Stainless coil is progressively made into a stainless steel pipe and then plasma welded. The pipes are cut to length and processed high tensile steel turnings are compressed into the interior of the pipe by a 400-t. press. The ends of the pipe are crimped and the resulting billets are fed through a walking beam furnace. When the billet reaches a certain temperature, the billet is rolled. The stainless steel cladding is evenly deposited along the surface and metallurgically bonded to the inner carbon steel core.

The rebar has a corrosion threshold of over 7 kg/cu.m chloride level and is expected to have a 75-100 year life. Epoxy coated rebar has a corrosion threshold of 0.7 - 1.2 kg/cu.m.

An average stainless steel clad thickness is 0.8mm. It is available in the size range of 13 mm (No. 4) to 32 mm (No. 10). Stelax produces Nuovinox 316L in diameters of 5/8 inch to 1.5 inches. The length available is from 20 ft to 38 ft long. Nuovinox rebar is also offered in fully fabricated form to the cutting and bending required, with ends sealed.

Nuovinox has a shear strength between the core and cladding of 300 Mpa when tested according to ASTM A 263-88. It is fatigue tested to 2 million cycles (150 Mpa - 275 Mpa) with no impairment to the metallurgical bond.

Ends can be sealed by welding or by application of stainless steel or plastic caps prefilled with a suitable sealant.

Testing Performed

Stelax conducted tests on their rebar. Their certificates are based on laboratory tests on regular batch samples taken from different rollings. All tests performed passed the required specifications. These results are found in Appendix B.

Midwest Industrial X-Ray, Inc. located in Fargo, North Dakota tested a sample #5 stainless steel clad rebar. A tensile, microetching and chemical spectrographic test was performed. The tensile test was completed per ASTM A2633,10. The microetching test was completed per ASTM E 488-18. The chemical spectrographic test was completed per ASTM E415-95a and ASTM E 1019-94. All tests passed the required specifications. Appendix C gives the results of these tests.

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<u>Cost</u>

The following is a breakdown of the costs associated with the stainless steel clad rebar. The fabrication includes the cutting and bending of the rebar by the supplier.

Structural Rebar 44,000 pounds Rebar is \$0.59 per pound Fabrication is \$0.12 per pound Freight estimated at \$2,000.00 Total cost of Material: <u>\$33,240.00</u>

The following are costs associated with the control structure using the epoxy coated

rebar. The total cost includes fabrication. Structural Rebar 40,942 pounds Rebar is \$0.74 per pound Total cost of Material: <u>\$30,297.08</u>

Construction

Site Visit 1.

An on-site evaluation was performed on June 4, 2001 to visually inspect the stainless steel clad rebar. The findings are as follows:

A. Bent bars are not uniformly bent.

B. Bent bars supplied are not fabricated to dimensions detailed in the project plans. The "k" bar legs are too long. This may require cutting of the bars and subsequent treatment such as capping or welding. Depending on the locations of the bars, this may result in an increase in contractor labor.

C. No. 5 bars were substituted for No. 4 bars in shipping.

D. Bent bars do not show signs of cracking or wrinkling of cladding at the bends.

E. The inner carbon steel bars appear to be wrapped with stainless steel cladding. Possible variations in diameter of the inner carbon steel bar may result in a raised seam in the cladding

material. See Photo 3. Damage to this seam produces an opening in the stainless steel cladding and entry point for moisture and corrosive materials to come into contact with the carbon steel bar.

F. Cuts and breaks were identified in the stainless steel cladding



Photo 2. Split in Stainless Steel Cladding (Notice the raised seems)

which exposes the inner carbon steel bar. See Photo 2, 3 and 4.

It was also noted that the stainless steel clad rebar was shipped on flatbeds and was strapped on by chains. Stelax Limited had specified that chains were not to be used by the hauling companies. As a result of the chains, some rust residue had formed on the rebar.



Photo 3. Cut in Stainless Steel Cladding



Photo 4. Split in Stainless Steel Cladding near a bend

The Valley City District personnel identified 30 k-type bent bars that were damaged. Stelax provided a welding procedure (compiled by a welding engineer in Alberta Canada) for repair of the damaged bars. The welding procedure for end-sealing and cladding repair of 316L Nuovinox rebar was in accordance with DIN 1733; 1736; and DIN 8556 for welding stainless steel clad plate.

Site Visit 2

An on-site evaluation of the stainless steel clad rebar being placed in the bridge deck was conducted on June 14, 2001. See Photos 5 & 6.



Photo 5. Bridge Deck Forms



Photo 6. Placement of Stainless Steel Clad Rebar

The following was observed from the site visit:

Α. Thekbars were cut to proper lengths as specified in plans and end welded. See Photo 7. All В. damaged rebar were welded to prevent unnecessary corrosionfrom occurring. See Photo 8. C. All spacers,

tie bars and material used within the bridge deck was that of stainless steel.



Photo 7. k-type bar cut and welded



Photo 8. Split rebar welded

The bridge deck was poured June 15, 2001. See Photos 9 & 10.

Photos 11 & 12 show the completed bridge deck.

Progress of the bridge deck will continue to be monitored. Visual inspection will be conducted to further study the use of stainless steel clad rebar. Photos 13-

15

depicts the construction and final product of the controlbridge with epoxy steel.



Photo 9. Bridge deck being poured



Photo 10. Bridge deck being poured



Photo 11. Finished bridge deck



Photo 12. Side view of finished bridge deck

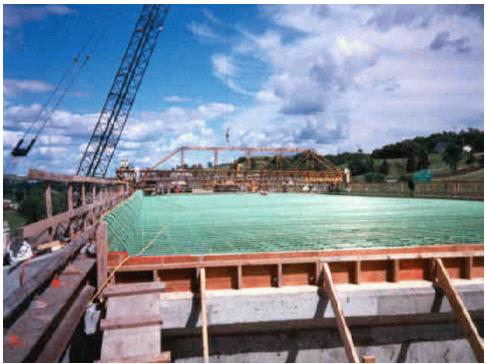


Photo 13. View of the control section bridge deck (epoxy coated rebar)



Photo 14. View of the control section bridge deck being poured



Photo 15. View of the control section bridge deck

Evaluation

The project will be evaluated at five, ten, fifteen, and twenty years.

Evaluation of the West Valley City Interchange bridge will be compared to the control structure.

<u>Summary</u>

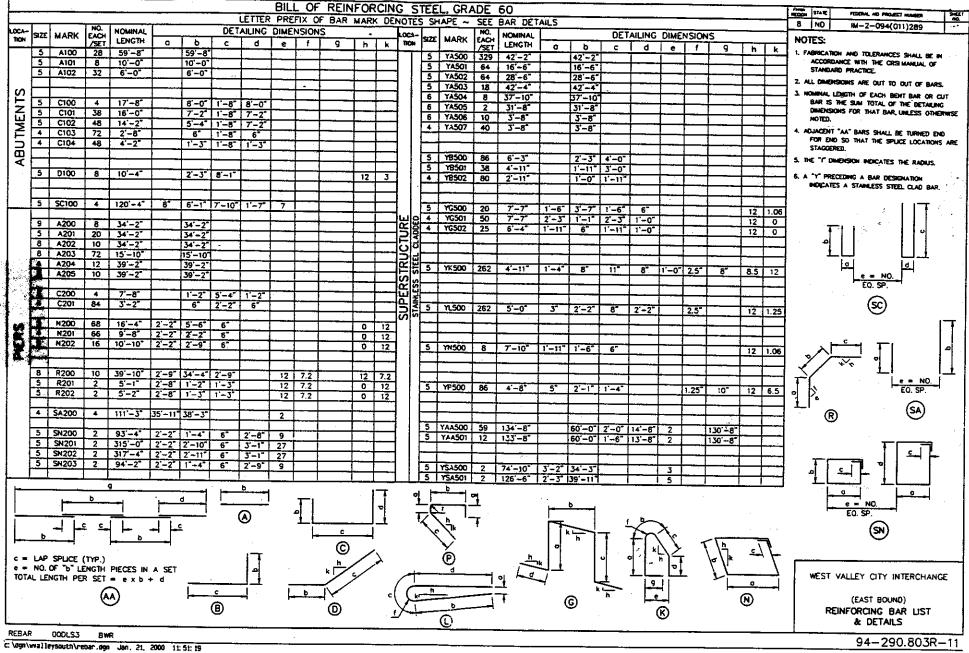
Comments from Mike Flaagen, NDDOT project engineer:

1. If we continue to use this material, we need to learn more about its characteristics. We need to know how to accept it in the field and look for irregularities in the coating.

2. The supplier should do a better job of bending the bars to the correct dimensions. Many of the bent bars were not exactly bent to the dimensions shown in the plans. This mainly affected installation because the bars were tougher to fit in place. In some cases the contractor had to cut bars to the correct length and cap them.

Other than these comments, Mike Flaagen reported that no other differences were noticed in construction using the stainless steel clad rebar.

Appendix A



Appendix B



STELAX (UK) LIMITED

The Wern Works. Briton Ferry Neath, SA11 2JX South Wales, UK

Ph: +44 1639 820 666 Fx: +44 1639 813 020 www.stelax.com email: nino@stelax.com

TO: Mr Tom Bold-NDDOT	
From: Nino Cacace.	
Fax:701-328-6913	
Date: 11-06-01	

Dear Tom.

Re : Test Certificates & bars to be repaired.

Please find attached 2 relevant test certificates. These certificates are based on our laboratory tests on regular batch samples taken from different rollings as per attached typical laboratory reports.

We were surprised and apologise for the 30 odd faulty bars shipped to you, which to us is a high number of rejects.

We rolled these bars last year in November/December before we could install our double-roller guide boxes, which is standard rolling practice for the final rolling stand (where the notches are formed) which ensures that the bar being rolled is centrally fed into the rolls very precisely. Any mis-guiding will cause the bar to be "pinched" on the one side along the longitudinal rib, presenting with a continuous or intermittent "flashing" on that side. Although not desirable in conventional rebar, cladded rebar is more delicate during hot rolling because of the potential damage to the ss-cladding. Our rollings subsequent to January have however been with these double-roller guides and have in effect eliminated the problem.

Most of the North Dakota contract was acid-descaled through our new acid-descaling plant which we commissioned late last year. Our final quality control inspections are now carried out at least 2 days after acid-descaling has been completed allowing time for cladding faults to become visible. Our only explanation due to lack of experience in that the initial batches out of our new system, were inspected too soon after acid descaling, and hence our inspectors would have missed these cladding faults.

We can assure you that our present rollings have extremely few rejects which are mostly completely predictable from rolling conditions (such as temperature or a loose guide in the mill which requires tightening).

B-1

We can now guarantee 100% reject-free despatches with our now greater experience in the final quality control inspection after acid descaling.

Yours sincerely,

Nino

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<u>STELAX (U.K.) Ltd.</u> <u>LABORATORY TEST REPORT</u> <u>Q.C.F. 6</u>

SAMPLE INFORMATION CONTRACTOR

Sample Number:- AA 027

Rolling date:- 01-12-00

Description:-16mm Nuovinox Re-bar

۰.

Part Number:- T.B.A. Batch Number:- N / A

TEST RESULTS

TEST	SPEC	RESULT	PASS / FAIL
Dimensional			
Bar diameter Gap Notch height Notch spacing Notch angle	15.90mm 6.10mm max 0.71mm min 11.10mm max 45° min	16.95mm 2.71mm 0.83mm 10.59mm 54°	pass pass pass pass pass pass
<u>Tensile</u>			
Yield strength Ultimate tensile strength Elongation %	420MPa min 620MPa min 9% min	' 546MPa 792MPa 13%	pass pass pass
Weight			
Kg/M	1.567Kg/ _M (nominal)	1.946Kg/M	pass
<u>Bend test</u>	No cracking of clad on Outside radius. No Wrinkling of clad on Inside radius.	No cracks No wrinkling	pass pass
Cladding	•		
Thickness	175um min	0.85mm min	pass

 Thickness
 175um min
 0.85mm min
 pass

 Bonding
 No cracks / delaminating
 No cracks / delaminating
 pass

Comments:-

Note:- Bend test must be performed against longitudinal rib.

Date:- 19-12-00	Signed:-	Saha	
<u>Date: 17 12 vv</u>	(Lab	oratory Supervisor)	

Report Nº 00035

STELAX (U.K.) Ltd. LABORATORY TEST REPORT Q.C.F. 6

SAMPLEINEORMATION

Sample Number:- AA 026

Part Number:- T.B.A.

Rolling date:- 01-12-00

Description:-16mm Nuovinox Re-bar

Batch Number:- N / A

TEST RESULTS

TEST	SPEC	RESULT	PASS / FAIL
Dimensional			
Bar diameter Gap Notch height Notch spacing Notch angle	15.90mm 6.10mm max 0.71mm min 11.10mm max 45° min	17.00mm 3.13mm 0.88mm 10.66mm 54°	pass pass pass pass pass
Tensile			
Yield strength Ultimate tensile strength Elongation %	420MPa min 620MPa min 9% min	541MPa 810MPa 22%	pass pass pass
<u>Weight</u>		,	
Kg / M	1.567Kg/ _M (nominal)	1.993Kg/ _M	pass
Bend test	No cracking of clad on Outside radius. No Wrinkling of clad on Inside radius.	No cracks No wrinkling	pass pass
<u>Cladding</u>			
Thickness Bonding	175um min No cracks / delaminating	0.80mm min No cracks / delaminating	pass . pass
Comments:- Note:-1	Bend test must be performe	d against longitudinal rib	

Note:- Bend test must be performed against longitudinal rib.

Date:- 19-12-00	Signed:-	8AL	
	(Lal	boratory Supervisor)	

B-5

Report Nº 00034

STELAX (U.K.) Ltd.

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LABORATORY RE-BAR TEST

RECORD SHEET

<u>Q.C.F. 5-1</u>

Batch Number:-	N/A	Bar Number:-	LAST	OFE	
Part Number:- T.B.A	L.	Description:- 10	mm Nuovinc	x Re-Bar	

Bar diameter	15.90mm	17.05 mm	Pass
Gap	6.10mm max.	2.99 mm	w state
Notch height	0.71mm min.	0.81 mm	~~~~
Notch spacing	11.10mm max.	10.65 mm	
Notch angle	-45° min.	54'	~
field strength	420 MPa min.	549 MPa	
J.T.S.	620 MPa min.	802 MPa	Aaso
Elongation %	9% min.	187	<u> </u>
Veight (Kg/M)	1.567Kg/M (nominal).	2.000 Kg/m	Pass
Bend test	No cracking of clad on conside radius. No winkling of clad on inside radius.	NO CRACKS NO WRINKLING	Pass
Clad thickness	175 um min.	0.70.44	
Clad bonding	No cracks / delaminating.	D-70 MM MIN Nº CAACKS Nº DECAMINATION	Pass

Satisfactory

3. . .

Signed:-(Laboratory Technician)

Report Nº A00038

Date:- 03-11-00

Q.C.F. S-L: Page 1 of 1 Review invol.2. Jacoust 02-11-00 **B-6**

<u>STELAX (U.K.) Ltd.</u> LABORATORY RE-BAR TEST <u>RECORD SHEET</u> <u>Q.C.F. 5-2</u>

Batch Number:-	N/A	Bar Number:- 25
Part Number:- T.B.A	4.	Description:- 19mm Nuovinox Re-Bar.

TEST SPEC'N RESULT PASS/FAIL

Bar diameter	19.10mm (Nominal)	20.00 mm	Pars
Gap	7.30mm max.	3.58 mm	~
Notch height	0.97mm min.	1.28 mm	~
Notch spacing	13.30mm max.	11.93mm	· ~~
Notch angle	45° min.	54.	~

Yield strength	420 MPa min.	SOT MPa	Pass
U.T.S.	620 MPa min.	694mPa	~
Elongation %	9 % min.	20%	~

			······································
Weight (Kg/ _M)	2.236Kg/M (nominal).	17.6171014	Fal
Weight (IEB/M)		2.617Kg/m	

Bend test	No cracking of clad on outside radius. No	NO CRACKS	~
·: ·		NO LAINKLING	1-ceps

Clad thickness	175 um min.	0 80 mm min	Pary	
Clad bonding	No cracks / delaminating.	NO CRACES		Ĺ

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Comments:-

Set Exactory

Date:- 13 - 11 - 00

Signed:-(Laboratory Technician)

Report Nº A00007

STELAX (U.K.) Ltd. LABORATORY TEST REPORT O.C.F. 6

SAMPLE INFORMATION NO.

Sample Number:- AA 028

Rolling date:- 01-12-00

Description:-16mm Nuovinox Re-bar

Part Number:- T.B.A. Batch Number:- N / A

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TEST RESULTS

TEST	<u>SPEC</u>	RESULT	PASS / FAIL
Dimensional			
Bar diameter Gap Notch height Notch spacing Notch angle	15.90mm 6.10mm max 0.71mm min 11.10mm max 45° min	16.88mm 2.50mm 0.87mm 10.62mm 54°	pass pass pass pass pass
<u>Tensile</u>		· · ·	
Yield strength Ultimate tensile strength Elongation %	420MPa min 620MPa min 9% min	547MPa 802MPa 13%	pass pass pass
<u>Weight</u>		,	
Kg/M	1.567Kg/M (nominal)	2.000Kg/ _M	pass
Bend test	No cracking of clad on Outside radius. No Wrinkling of clad on Inside radius.	No cracks No wrinkling	pass pass
Cladding	·· · .	- <u>N</u>	
Thickness Bonding	175um min No cracks / delaminating	0.95mm min No cracks / delaminating	pass pass ::
Comments:- Note:-	Bend test <u>must</u> be performe	d against longitudinal rib.	· .
Date:- 08-12-00		Signed:-	_
<u>~~~~~</u>		(Laboratory Supervi	sor)

Report Nº 00036



Appendix C

MIDWEST HOUSTPLAL X-RAY, DIC.

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Midwest Industrial X-Ray, I	nc.		
NONDESTRUCTIVE TESTING			
P.O. BOX 133 - 4032 - 7TH AVENUE NORTH			
FARGO, NORTH DAKOTA 58107		BRANC	I OFFI
SONIC PENETRANT ITIC PARTICLE ITIC PARTIFICATION ITIY ASSURANCE		MINNEA COUNCIL	
Lurgical Investigations s relieving	` _		
REPORTED TO: N.D. DOT	INVOICED	TO:	
	Same		
Fargo, ND			
			1 1 5
PROJECT NAME AND LOCATION: PROJECT NO .:	INVOICE	INVOICE	
# 5 Stainless Steel Rebar	DATE:	NUMBER	
	6/20/01	9135	
DESCRIPTION:	AMOUNT:		
Tensile Test	\$171.00		
Microetch	31/1.00		
Spectrographic	Pay last ar	nount in	•
All accounts due on the 10th of month following purchase. A finance charge of 1 1/2 % will be made on accounts over 30 days past due, which is an	this colum		
annual percentage rate of 18%		-	
			-
7,3,12			
Tensile Test	-		
1 @ \$18.00 / test	\$18.00	<u> </u>	-
8.5 Microetch	_		•
8.5.1 Microetch Analysis	\$28.00		-
1 @ \$28.00 / each			-
8.6 Chemical Spectrographic	-		-
8.8.1 Analysis	\$125.00)	-
1 @ \$125.00 / each			-
			- .
	1		-
	1		-
			-
			-
		<u></u>	-
			-
	1		-
			-
			<u>~</u>
PLEASE PAY FROM THIS INVOICE & RETURN YELLOW COPY.			-
Thank you. TOTAL:	\$171.00)	

C-1

MIDWEST INDUSTRIAL X-RAY, INC.



- RADIOGRAPHY - ULTRABONIC

TELEPHONE (701) 282-7846 FAX (701) 282-6711

Midwest Industrial X-Ray, Inc.

NONDESTRUCTIVE TESTING

P.O. 80X 133 - 4032 - 7TH AVENUE NORTH FARGO, NORTH DAKOTA 58107

BRANCH OFFICES

MIDWEST INDUSTRIAL X-RAY, INC.

FARGO, ND



TELEPHONE (701) 282-7846 FAX (701) 282-6711



P.O. BOX 133 - 4032 - 7TH AVENUE NORTH FARGO, NORTH DAKOTA 58107



MINNEAPOLIS, MN COUNCIL BLUFFS, JA

- · RADIOGRAPHY ULTRASONIC LIQUID PENETRANT
- MAGNETIC PARTICLE
- WELDER CERTIFICATION A QUALITY ASSURANCE METALLURGICAL INVESTIGATIONS STRESS RELIEVING STRESS RELIEVING

Date: 6/20/01

Test For: N.D. DOT

Material: #5 plated rebar

Base Dimensions and Loading

Sample:	Diameter (in)	Yield (bi)	Ultimate (Ibf)
1	0.625	25800	38500
Stress:	Area (in ²)	Yield (psi)	Ultimate (psi)
1	0.3068	84095	12549Q
Elongation:	Base (in)	Final (in)	%
1	8.00	9.50	18.8

Platting range of thickness:

.031 - .127 inch

C-2

MIDWEST INDUSTRIAL X-RAY, UNC.



· RADIOGRAPHY

ULTRASONIC

- LIGUED FENETRANT HAGNETIC PARTICLE - WELDER GERTIFICATION 6 QUALITY ASSURANCE - METALLURGICAL INVESTIGATIONS - STRESS RELEVING - X-RAY

P.03

TELEPHONE (701) 282-7846 FAX (701) 282-8711

Midwest Industrial X-Ray, Inc.

NONDESTRUCTIVE TESTING

P.O. BOX 133 - 4032 - 7TH AVENUE NORTH FARGO, NORTH DAKOTA 58107

BRANCH OFFICES

MERINEAPOLIS, MN COUNCIL BLUFFS, IA

Date: 6-20-01

Test For.

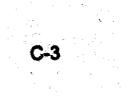
Material: #5 plated rebar

Base Dimensions and Loading				
Sample:	Diameter (in)	Yleid (ibf)	Ultimate (lbf)	
1	0.625	25800	38500	
<u>stress;</u>	Area (in2)	Yield (psi)	Ultimate (psl)	
1	0.3068	84095	125490	
<u>Elogation:</u>	Base (in)	Final (in)	%	
1	8.00	9.50	18.8	

Platting range of thickness: .031 - .127 inch

Microetching: ASTM E 488-18

Tensile ASTM A2633,10



MIDWEST INDUSTRIAL X-RAY, INC.



· RADIOGRAPHY

Midwest	Industrial	X-Ray,	Inc.
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NONDESTRUCTIVE TESTING

P.O. BOX 133 - 4032 - 7TH AVENUE NORTH FARGO, NORTH DAKOTA 58107

BRANCH OFFICES

MINNEAPOLIS, MN COUNCIL BLUFFS, IA

÷	ULTRASONIC
•	Liquid Penetrant
	MAGNETIC PARTICLE
-	WE ARE CERTIFICATION

A QUALITY ASSURANCE
 METALLURGICAL INVESTIGATIONS
 STRESS RELIEVING

- X-RAY

Report to:	N.D.	DOT

Fargo, ND

Subject: Chemical analysis of sample received June 7, 2001

Sample Identification / Description: Steel Sample

Chemical Composition:

	%
Carbon	0.330
Manganese	0.990
Phosphorus	0.010
Sulfur	0.051
Silicon	0.230
Nickel	0.170
Chromim	0.240
Molybdenum	0.050
Copper	0.160
Aluminum	0.034
,	

Test Method: Carbon per ASTM E1019-94; Others per ASTM E415-95a

C-4

TELEPHONE (701) 282-7846

FAX (701) 282-6711

6/20/01

Date:

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Appendix D



Ph: +44 1639 820 666 Fx: +44 1639 813 020 www.stalax.com email: <u>nino@stalax.com</u>

STELAX (UK) LIMITED

The Wern Works, Briton Ferry Neath, SA11 2JX South Wales, UK

TO: Mr Tom Bold-NDDOT	
From: Nino Cacace.	
Fax:701-328-6913	
Date: 6-06-01	

Dear Tom,

Re : Your e-mail of the 6-6-01

We inspect all Nuovinox bars 100% before dispatch.

All bars especially bent bars are acid-pickled as a final step prior to inspection.

We regret the inconvenience and are standing by to receive your requirements in replacement bars which we shall courier to you.

Attached is a welding procedure, compiled for us by a welding engineer in Alberta.

Yours sincerely,

Antonino Cacace.

Weiding Procedure for End-Sealing and Cladding Repair 316L Nuovinox Rebar in Accordance With DIN 1733; 1736; and DIN 8556 for Welding Stainless-Steel Clad Plate.

1.0 PURITY & WELD PREPARATION.

- 1.1 At all times contamination from Carbon Steel must be avoided such as dragging Nx bars across carbon steel material or worktops. Weld flattening, Pick Hammers and brushes for finishing the weld must be stainless steel.
- 1.2 Avoid contamination from sulfur. Grinding and Cutting Discs with sulfur free binder must be employed (Synthetic Resin Bonding) when cutting or grinding.
- 1.3 Weld Area must be cleaned and all rust or flashings removed. No oil or grease must be present.

2.0 PREHEATING.

2.1 No Pre-heating is required.

3.0 WELDING PROCESS.

3.1 TIG welding with cold wire and a straight Argon shield @ 35CFM.

4.0 END SEALING.

4.1 A 2-Layer welding procedure is required to avoid possibility of weld dilution by the carbon steel core at the surface of the end-seal.

4.2 The initial "Buffer Layer" should be with a 309L wire of diameter 3/32" (ER309L ASME SFA 5.9) and a setting of 55AMPS.

4.3 The final layer is to be 316L (ER316L ASME SFA5.9) with a diameter 1/16" and a setting of 55AMPS

The welding technique is to initiate at the outside circumference of the cross section ; gradually spiraling from the outside to the centre until fully welded.

5.0 CLADDING REPAIRS:

5.1 Hair-line cracks should be repaired with a single welding layer of 316L 1/16" diameter & a setting of 35AMPS. All other settings remain the same.

6.0 POST HEAT-TREATMENT.

6.1 None.

7.0 WELD-SEAM AFTER-TREATMENT.

7.1 Wire brushing.

8.0 INSPECTION. 8.1 Visual for pin-holes.

Approved by :

W. Hamilton P.Eng.

Hamilton Engineering 12203-41 Ave. NW Edmonton. Alberta T65 0V6